

Effect of Ultrasonic Peening on Microhardness and Residual Stress in Materials and Welded Elements

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ABSTRACT

The development of the Ultrasonic Peening (UP) technology was a logical continuation of the work done before directed on the investigation and further development of known techniques for surface plastic deformation such as shot peening, hammer peening, needle peening etc. The UP technique is based on the combined effect of the high frequency impacts of the special strikers and ultrasonic oscillation in treated material. The UP was applied successfully for the increasing of the fatigue life of parts and welded elements, eliminating of distortions caused by welding and other technological processes, residual stress-relieving, increasing of the hardness of materials. The results of fatigue testing showed that UP is the most efficient technique for increasing the fatigue life of welded elements as compared to such existing improvement treatments as grinding, TIG-dressing, shot peening, hammer peening, etc. An overview of the UP technology is given with the initial results of investigation of microhardness and residual stresses in UP treated materials and welded elements discussed as well in this paper.

1. Introduction.

Ultrasonic Peening of parts and welded elements is a comparatively recent and promising technology that has emerged from extensive development by engineers mostly from Ukrainian and Russian research institutes. The Ultrasonic Peening (UP) produces a number of beneficial effects in metals and alloys. Foremost among these is increasing the resistance of materials to surface-related failures, such as fatigue and stress corrosion cracking. One of the promising ways of industrial application of UP is the post-weld treatment of welded elements and structures. The results of fatigue testing showed that UP is the most efficient and economical technique for increasing the fatigue life of welded elements as compared to such existing improvement treatments as grinding, TIG-dressing, shot peening, hammer peening etc.

The development of the UP technology was a logical continuation of the work done before directed on the investigation and further development of known before techniques for surface plastic deformation such as shot peening, rolling, hammer peening etc [1]. During the different stages of its development the UP process was also known as "ultrasonic treatment", "ultrasonic impact technique/technology", "ultrasonic impact peening" or "ultrasonic impact treatment".

The modern equipment for UP is based on known technical solutions of working heads for hammer peening known from 40's. At that time and later a number of different multi-strikers working heads were developed for impact treatments of parts and welded elements by using mostly pneumatic driven equipment. In order to more effectively perform the treatment of parts and welded elements by using pneumatic and other types of equipment, the special strikers made of high-strength materials are used. The effective impact treatment is provided when the strikers are not connected to the tip of actuator but are located between the actuator and treated material.

For the first time, the possibility of using ultrasonic technology for improving the service properties of welded structures was described in 1959 by A.V. Mordvintseva [3]. She analyzed the using of ultrasonic treatment for relieving of welding residual stresses.

Initially in the equipment for ultrasonic treatment the deforming elements-strikers were attached to the tip of the ultrasonic transducer [3,4]. In this case the ultrasonic contact with the metal surface is provided by a whole instrument with the force of 100 - 500 N. Such ultrasonic systems can be used, for example, for finishing treatment of metal surfaces. More effective surface deformation by using of the energy of ultrasound is achieved when the strikers are not connected with ultrasonic

transducer but are located near the transformer's tip. This technique was proposed in former Soviet Union and USA at the end of 60's [5-9] and, later, different types of ultrasonic equipment were developed based on this idea. In the case of so-called "intermediate" element-striker the force of 30 - 50 N is required for treatment of materials.

At the end of 60's and beginning of 70's the intensive investigation of the influence of high power ultrasonics on the properties of materials and welded elements was initiated at the Institute of Metal Physics (Kiev, Ukraine) [10-12]. The intermediate element-striker was employed for surface strengthening and plastic deformation of materials. This striker oscillated in the gap between the end of the ultrasonic transducer and treated specimen. The changes in the mechanical properties of the materials and texture under the action of the ultrasonic treatment were analyzed [13]. The results of these studies initiated the development of the UP technology. Practically, at the same time the efficiency of the application of intermediate element during ultrasonic treatment for plastic deformation of materials was analyzed in the number of research centers in former USSR and USA [5-18].

At the very beginning of 70's the collaboration between the Paton Welding Institute (PWI) and the Institute of Metal Physique (IMP) in the application of high power ultrasonics and high frequency impacts for improvement treatment of welded elements and structures and relieving residual stresses was started. The first results of this collaboration in the field of ultrasonic impact treatment of welded elements and structures were published in 1974 [14] and later [15, 17-21].

In 1982 the PWI intensifies its efforts in the development of the application of ultrasonic impact technology for increasing the fatigue life of welded elements and structures. For the first time the PWI proposed to use UP for treatment of only the zone of transition from weld to base metal. The oscillating sphere was used for plastic deformation of weld toe creating the radius equals to the radius of sphere. This kind of UP treatment provided significant increase of the fatigue life of welded elements – from 15 to 20 times depending on the level of cyclic loading. The standard ultrasonic equipment USG-10 (power supply 10 kW) and vibrating sphere with the diameter 16 mm were used at that time for UP [22]. The formation of so-called "groove" in the weld toe zone for optimum fatigue life improvement of welded elements by UP was proposed by PWI [23,24]. Later, a number of industrial applications and other aspects of UP technology were developed at PWI. For example, the effectiveness of the UP application for the increase of the fatigue life of welded elements subjected to cyclic compression was analyzed by testing of large-scale welded elements of construction equipment as well as welded elements of bridges [23,25].

Starting form 1987 the results on the development of the UP technology were presented by PWI in some East European countries [26, 27] and later for western scientific and engineering communities [28-33].

In 1993 the results of the development of the UP technology and fatigue assessment of welded specimens after application of the UP were presented for the first time at the International Institute of Welding by the scientists form PWI [34]. Later, more results on the development of the UP technology and fatigue testing of welded specimens, specification for weld toe improvement by UP and also the results of the verification of the efficiency of the UP technology conducted in the frame of IIW test program were presented with participation of the PWI [35-37].

Presently, the field of high power ultrasonics enjoys a renewed interest, and intensive research and development activity in industrial application of high power ultrasonics and particularly ultrasonic impact technique are conducted in Ukraine, Russia, Canada, USA and China [38-44]. During such activity the principles of optimum UP application and corresponding software were developed. The technology and equipment for UP were adapted for different industrial applications. The Computerized Complex for UP of materials, parts and welded elements was developed recently based on using of the high efficient optimized piezoelectric transducers. The complex consists of the compact ultrasonic transducer, generator and laptop with expert system for UP optimum application: maximum possible increase in fatigue life of welded elements with minimum cost, labor and power consumption [45,46].

2. Enhancement of Engineering Properties of Materials and Welded Elements by Ultrasonic Peening

Intense levels of high frequency acoustic energy, or high power ultrasonics, have found practical use in many industrial processes. In most industrial applications, high power ultrasonics involves power levels of hundreds to thousands of watts, and ultrasonic systems operating in the frequency ranges from 15 kHz to 100 kHz. Typical amplitudes range from about 10 to 40 microns. Such ultrasonic system, for instance, operating at 20 kHz creates a cyclic acceleration of around 50,000 g (acceleration of gravity).

One of the promising directions in using of the high power ultrasonics for industrial applications is the Ultrasonic Peening (UP) of materials, parts and welded elements. The UP technique is based on the combined effect of the high frequency impacts of the special strikers and ultrasonic oscillation in treated material.

In the fatigue improvement the beneficial effect is achieved mainly by introducing of the compressive residual stresses into surface layers of metals and alloys, decrease in stress concentration of weld toe zones and the enhancement of the mechanical properties of the surface layer of the material. A schematic view of the cross section of material/part improved by UP is shown on Figure 1 and description of the UP benefits is presented in Table 1.

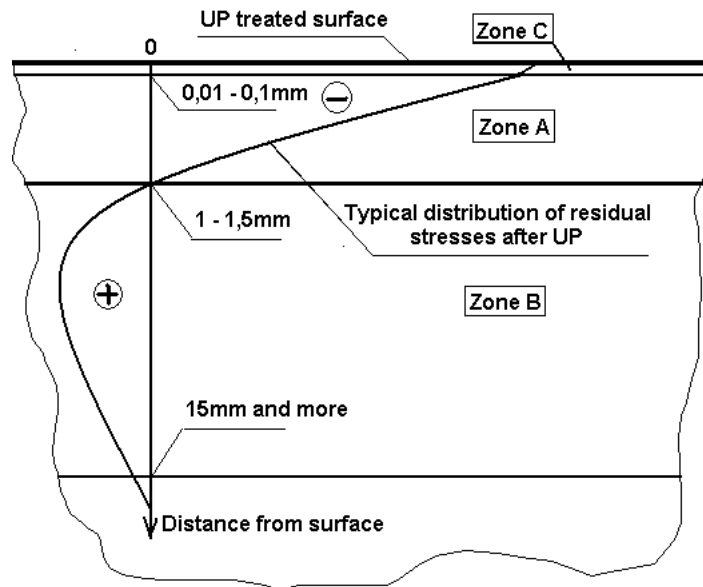


Figure 1. Schematic view of the cross section of material/part Improved by Ultrasonic Peening

Table 1. Zones of Material/Part Improved by Ultrasonic Peening

Zone	Description of zone	Penetration (distance from surface), mm	Improved characteristics
A	Zone of plastic deformation and compressive residual stresses	1 – 1,5 mm	Fatigue, corrosion, wear, distortion
B	Zone of relaxation of welding residual stresses	15 mm and more	Distortion, crack propagation
C	Zone of nanocrystallization (produced at certain conditions)	0,01 – 0,1 mm	Corrosion, wear, fatigue at elevated temperature

Figure 2 and Figure 3 show the concept of the fatigue life improvement of welded elements by UP. In case of welded elements for significant increase of the fatigue life it is enough to treat only the weld toe zone – the zone of transition from base metal to the weld and to produce of the so-called groove [23, 24].

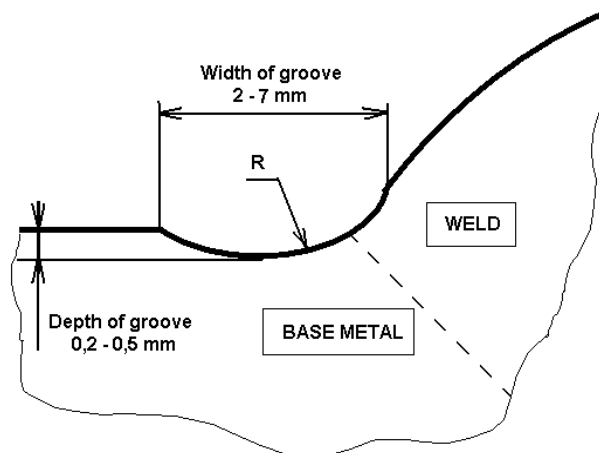


Figure 2. Profile of weld toe improved by Ultrasonic Peening

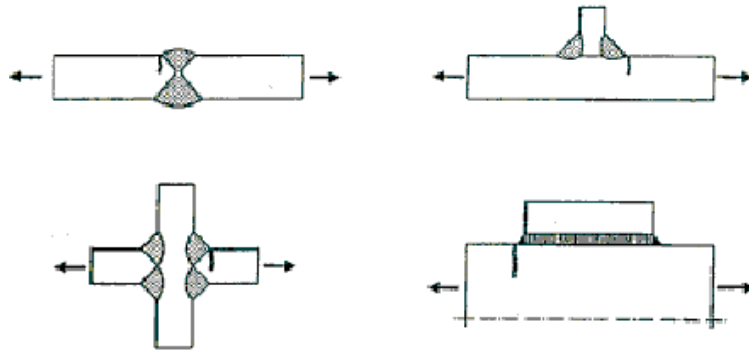


Figure 3. Examples of welded elements suitable for Improvement
(in accordance with IIW Doc. XIII-1815-00)

3. Equipment for Ultrasonic Peening

There are two general types of ultrasonic transducers which can be used for UP: magnetostrictive and piezoelectric. Both accomplish the same task of converting alternating electrical energy to vibratory mechanical energy but do it in a different way (Figure 4). In magnetostrictive transducer the alternating electrical energy from the ultrasonic generator is first converted into an alternating magnetic field through the use of a wire coil. The alternating magnetic field is then used to induce mechanical vibrations at the ultrasonic frequency in resonant strips of magnetostrictive material.

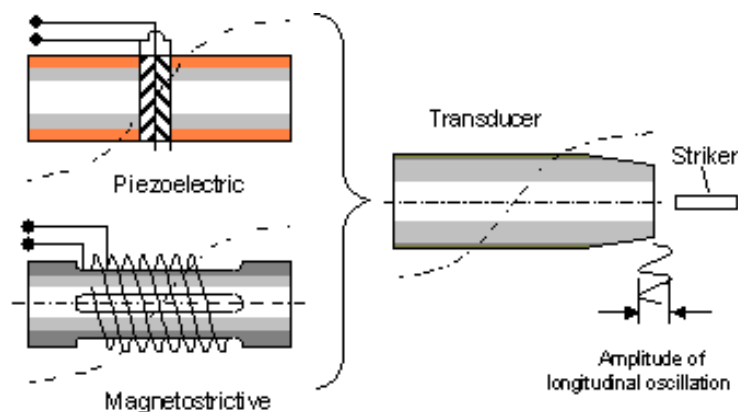


Figure 4. Schematic view of transducer for Ultrasonic Peening.

Magnetostrictive transducers are generally less efficient than the piezoelectric ones. This is due primarily to the fact that the magnetostrictive transducer requires a dual energy conversion from electrical to magnetic and then from magnetic to mechanical. Some efficiency is lost in each conversion. Magnetic hysteresis effects also detract from the efficiency of the magnetostrictive transducer. In addition, the magnetostrictive transducer for UP needs forced water-cooling. The equipment in this case is relatively heavy and expensive.

Piezoelectric transducers convert the alternating electrical energy directly to mechanical energy through the piezoelectric effect. Today's piezoelectric transducers incorporate stronger, more efficient and highly stable ceramic piezoelectric materials, which can operate under the temperature and stress condition. Piezoelectric transducers are reliable today and can reduce the energy costs for operation by as much as 60%.

Due to the high energy efficiency of piezoelectric transducers the effect in fatigue life improvement is practically the same by using of the magnetostrictive transducer with power consumption of 1000 Watts and optimized piezoceramic transducers with power consumption of only 250 Watts (Figure 5).

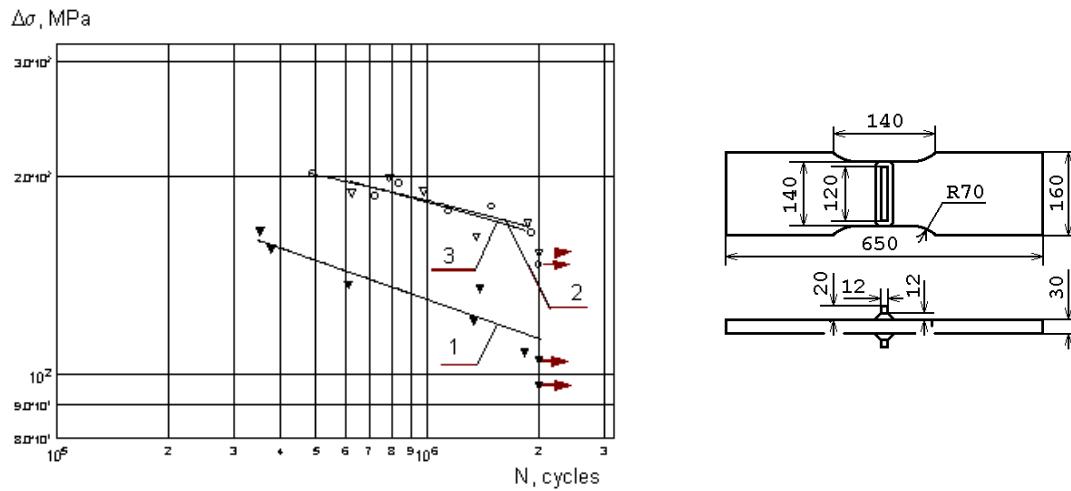


Figure 5. Fatigue curves of non-load carrying fillet welded joint:
 1 - in as-welded condition;
 2 and 3 - after application of the UP by using magnetostriuctive transducer ($P = 1 \text{ kW}$) and optimized piezoelectric transducer ($P = 0,25 \text{ kW}$)

A Computerized Complex for UP of materials, parts and welded elements was developed recently based on using of the high efficient and reliable piezoelectric transducers. The Complex consists of the compact ultrasonic transducer, generator and laptop with Expert System for UP optimum application (Fig. 6).



Figure 6. Computerized Complex for Ultrasonic Peening of parts and welded elements

4. Effect of Ultrasonic Peening on Microhardness of Materials

The effect of the UP treatment on the microhardness of metal: a widely used engineering material, the AISI 304 stainless steel was considered. A distribution of microhardness as a function of the depth – distance from the treated surface of material was analysed.

4.1 Samples

The material used was an AISI 304 stainless steel with the following chemical compositions: 0.08 C, 18.20 Cr, 8.60 Ni, 1.10 Mn, 0.60 Si, 0.020 P, 0.010 S and balanced Fe. Two cross-sectioned samples from the AISI 304 were prepared. In

the first sample a plane square area of 25mm x 25mm was subjected to a UP treatment. The second sample was used to produce by UP so-called “groove” which is used fatigue life improvement of weld toe zone. After the UP treatment the samples were cross sectioned, moulded in a resin, and then polished to be as smooth as possible for the microhardness tests.

4.2 Measurement of Microhardnes

A Digital Microhardness Tester MMT3 (Buelher) was used with the Vickers indenter to determine the Hardness Vickers of the UP treated samples. The procedure followed the standard ASTM E384-89 (Standard Test Method for Microhardness of Materials). The value of the test load was 100 gf and it lasts 15 sec. The distance between each indentation was minimum 3 times the length of the main diagonal of the indentation, as indicated in the standard.

4.3 Results

4.3.1 The groove sample

The profile of microhardness in the sample with the “groove” produced by UP is presented on Figure 7.

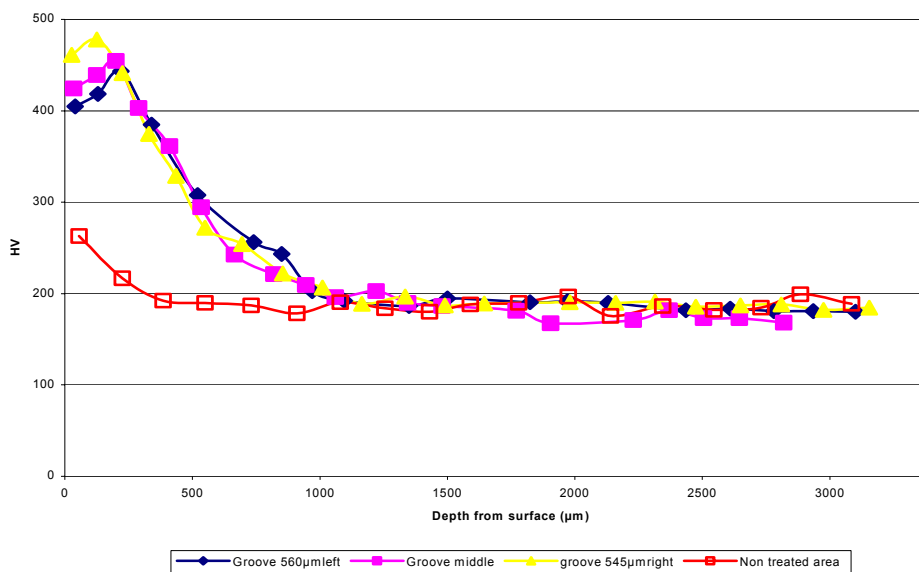


Figure 7. Profile of microhardness distribution in the different locations of the sample with the “groove” produced by Ultrasonic Peening

It could be seen, that the microhardness in the bottom of the groove is significantly higher than in a non-treated area near the top surface layer (the largest difference is about 200 at the depth of 150µm). There is an insignificant increase of microhardness with the increase of the depth for the first 200 µm and then, the microhardness decreases to be stabilized at nearly 1000-1500µm in depth.

4.3.2 The plane sample

The profile of microhardness in the plane sample after UP is presented on Figure 8. Data presented on figure 7 and Figure 8 show that the depth of plastic deformation zone after UP treatment is 1 - 1,5 mm.

5. Residual Stress Measurement

Residual stresses are one of main factors determining the efficiency of Ultrasonic Peening in fatigue life improvement. The results of residual stress measurement by different experimental techniques in the UP treated specimens are presented on Figure 9-12.

5.1. Ultrasonic Method

Ultrasonic method [47] was used for residual stress measurement in the model of welded element – plate with the welded bead on one side (Figure 9). Averaged through thickness of plate residual stresses were measured by using bulk ultrasonic waves before and after UP of the welded bead. The distribution of residual stresses along the width of specimen in this case imitates the in-depth distribution of residual stresses after UP of real welded joint.

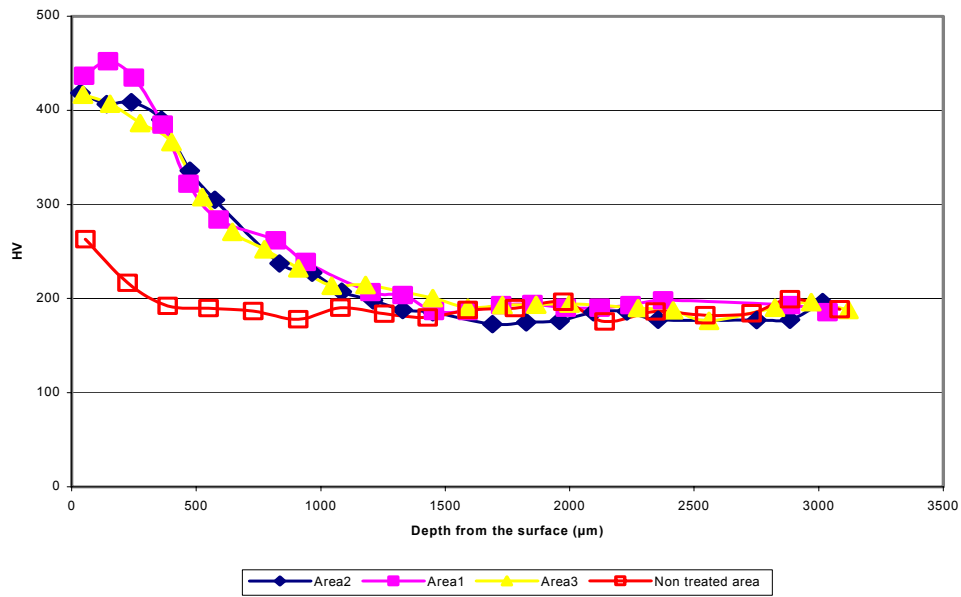


Figure 8. Profile of microhardness distribution in the different locations of the plane sample after Ultrasonic Peening.

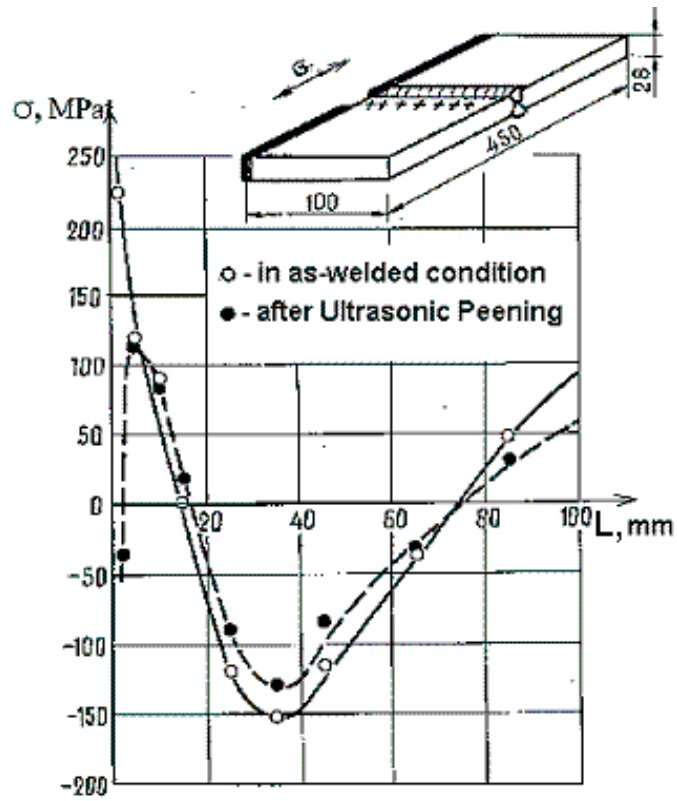


Figure 9. Distribution of residual stresses (averaged through thickness) in the model of welded element before (○) and after (●) Ultrasonic Peening

5.2. X-Ray Method

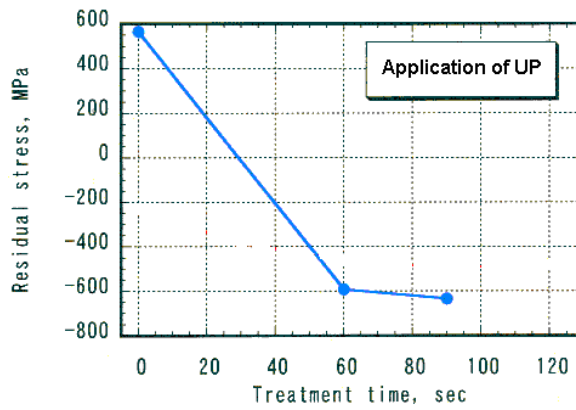


Figure 10. Relieving of induced by EDM harmful tensile residual stresses and introducing of beneficial compressive residual stresses in surface layers of material by Ultrasonic Peening

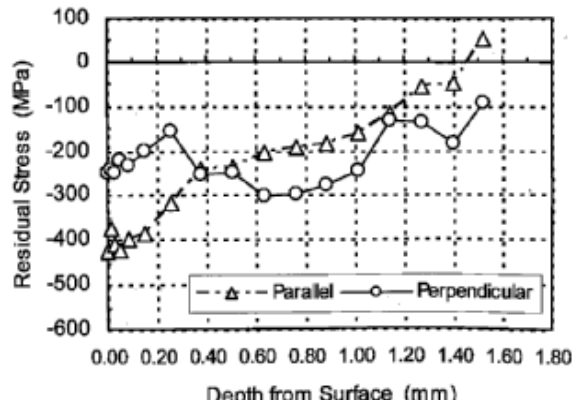


Figure 11. Distribution of residual stresses depending on the distance from the treated surface of material after ultrasonic impact treatment [42].

5.2. Neutron Diffraction Method

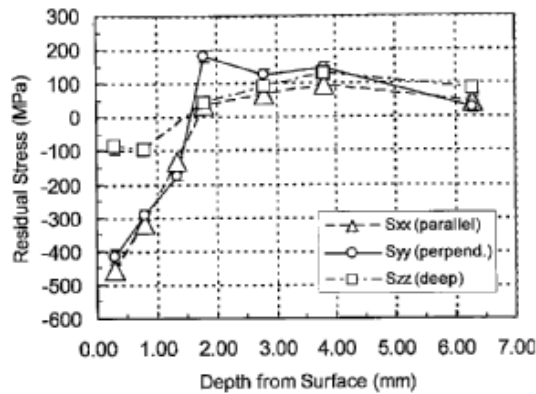


Figure 12. Distribution of residual stresses depending on the distance from the treated surface of material after ultrasonic impact treatment [42].

The results of residual stress measurement by different techniques show that UP causes relieving of harmful tensile residual stresses and inducing beneficial compressive residual stress with the depth of penetration of about 1,5 mm what is well correlated with the depth of plastic deformation determined by microhardness measurements.

Summary

1. One of the promising directions in using of the high power ultrasonics for industrial applications is the Ultrasonic Peening (UP) of materials, parts and welded elements. The UP technique is based on the combined effect of the high frequency impacts of the special strikers and ultrasonic oscillation in treated material. The unique mechanism of UP and developed compact equipment provide the highest increase in fatigue life of welded elements as compared with the application of existing improvement treatments such as grinding, TIG-dressing, shot peening, hammer peening.
2. An advanced computerized complex for UP of parts and welded elements was developed recently based on using of the piezoelectric transducer. The complex consists of the compact ultrasonic transducer, generator and laptop with Expert System for UP optimum application: maximum possible increase in fatigue life of welded elements with minimum cost, labor and power consumption.
3. The UP provide efficient relieving of harmful tensile residual stresses and inducing of beneficial compressive residual stresses as well as increase in microhardness of the surface layers of material. The depth of plastic deformation zone after UP is approximately the same as the depth of induced compressive residual stresses: 1-1,5 mm.
4. The developed computerized complex for UP could be used in different applications for increasing of the fatigue life of parts and welded elements, eliminating of distortions caused by welding and other technological processes, residual stress relieving, increasing of the hardness of the surface of materials and surface nanocrystallization.

6. References

1. Trufyakov V. I., Mikheev P. P., Kudryavtsev Y. F. Fatigue Strength of Welded Structures. Residual Stresses and Improvement Treatments. London. Harwood Academic Publishers GmbH. 100 p., 1995.
2. Мордвинцева А.В. Обработка сварных соединений ультразвуком с целью снятия остаточных напряжений. Применение ультразвука в сварочной технике. - М.: ЦИНТИЭнергомаш, 1959. - с.32-43. - (Тр. МВТУ им.Н.Э.Баумана; вып.45) (Treatment of welded joints by ultrasound with the goal of residual stress relieving).
3. Muhanov I. I. and Golubev Y. M. Hardening of steel-wares by ball that vibrates with ultrasonic frequency. *Vestnik Mashinostroeniya*. №11. -P. 52-53. 1966 (in Russian).
4. Holopov Y.V. Treatment of metal welded joints by ultrasound aimed on residual stress decreasing. *Svarochnoe Proisvodstvo*. №12.-P. 200-203. 1973 (in Russian).
5. Nerubay M.S. Influence of ultrasonic vibrations of instrument on cold-hardening and residual stress. *Vestnik Mashinostroeniya*. №10. -P. 65-67. 1968 (in Russian).
6. Krilov N. A., Polishchuk A. M. Using of ultrasonic apparatus for metal structure stabilization. *Physical background of industrial using of ultrasound. Part 1. LDNTP. Leningrad..- P. 70-79. 1970 (in Russian)*.
7. U.S. Patent No. 3,595,325. 1971. Intermediate Impact Device.
8. U.S. Patent No. 3,609,851. 1971. Metal Working Apparatus and Process.
9. K. Graff. Impact of a Spherical Tool against a Sonic Transmission Line. *The Journal of the Acoustical Society of America*. Volume 52, Number 1 (Part 2), 1972. pp. 254-259.
10. Полоцкий И.Г., Прокопенко Г.И., Трефилов В.И., Фирстов С.А. Действие ультразвука на дислокационную структуру монокристаллов молибдена. ФТТ. 1969, № 11, - С. 755-757. (Effect of ultrasonics on dislocation structure of molybdenum monocrystals)
11. Полоцкий И.Г., Прокопенко Г.И., Трефилов В.И., Фирстов С.А. Действие ультразвука на дислокационную структуру и механические свойства молибдена. ФММ. 1973 -35, № 6. - С. 1199-1205. (Effect of ultrasonics on dislocation structure and mechanical properties of molybdenum)
12. Ковш С.В., Полоцкий И.Г., Прокопенко Г.И., Трефилов В.И., Фирстов С.А. Влияние циклического деформирования на дислокационную структуру и механические свойства молибдена, хрома, вольфрама. Пробл. прочн. 1973, № 11.- С. 15 – 20. (Influence of cyclical deformation on dislocation structure and mechanical properties of molybdenum, chrome, wolfram)

13. Котко В.А., Прокопенко Г.И., Фирстов С.А. Структурные изменения в молибдене, наклепанном с помощью ультразвука. ФММ.- 1974.- 37. № 2.- С. 444-445. (Texture changes in the hammer-hardened molybdenum with the help of ultrasonics)
14. I. Polozky, A. Nedoseka, G. Prokopenko et al. Relieving of welding residual stresses by ultrasonic treatment. *The Paton Welding Journal*. 1974. № 5.- p. 74-75.
15. Полоцкий И.Г., Прокопенко Г.И., Трефилов В.И., Фирстов С.А. Действие ультразвуковых и низкочастотных колебаний на структуру и свойства сварных соединений молибдена // Сварочное производство.- 1975.- № 7.- С. 9 –11. (Action of ultrasonic and low-frequency vibrations on texture and properties of molybdenum welded joints)
16. Author's Certificate (USSR) # 472782. 1975. Ultrasonic head for strain hardening and relaxation treatment. E.Sh. Statnikov, L.V. Zhuravlev, A.F. Alexeyev, Yu.A. Bobylev, E.M. Shevtsov, V.I. Sokolenko and V.F. Kulikov..
17. Author's Certificate (USSR) # 601143. 1978. Ultrasonic multiple-strikers device. G. Prokopenko and V. Krivko.
18. Кривко В.П., Прокопенко Г.И. Ультразвуковая обработка сварных соединений // Сварочн. произв. – 1979.- № 5.- С. 32-33. (Ultrasonic treatment of welded joints)
19. Грузд А.А., Казимиров А.А., Недосека А.Я., Прокопенко Г.И. Влияние ультразвуковой обработки на структуру и свойства сплава АМг 6 // Автоматич. сварка. – 1980.- № 7.- С. 38 – 41. (Influence of ultrasonic treatment on texture and properties of АМг6 alloy)
20. Author's Certificate (USSR) # 777072. 1980. Method of surface hardening of parts. G. Prokopenko et al.
21. Author's Certificate (USSR) # 1261310. 1986. Method of treatment of parts made from titanium alloys. G. Prokopenko et al.
22. Михеев П.П., Недосека А.Я., Пархоменко И.В. et al. Эффективность применения ультразвуковой обработки для повышения сопротивления усталости сварных соединений. - Автоматическая сварка, 1984, №3. - с.4-7. (Efficiency of ultrasonic treatment application for increase of fatigue strength of welded joints)
23. Y.F. Kudryavtsev, V.F.Korshun and A.Z.Kuzmenko. Improvement of fatigue life of welded joints by the ultrasonic impact treatment. *Automatic Welding (Paton Welding Institute)*. 1989. No. 7. p.24-28.
24. Yu.F.Kudryavtsev, P.P.Mikheev, V.F.Korshun. Influence of plastic deformation and residual stresses, created by ultrasonic impact treatment, on the fatigue strength of welded joints. *Avtomaticheskaya Svarka*. 1995. No. 12. p.3-7.
25. A.G.Burenko, E.K.Dobukina, P.P.Mikheev, Yu.F.Kudryavtsev. Increase of fatigue resistance of load-carrying elements of welded structures subjected to action of cyclic compression. *Avtomaticheskaya Svarka*. 1993. No. 3. p.8-12.
26. V.I. Trufyakov, P.P. Mikheev, Yu.F. Kudryavtsev. Increasing of fatigue strength of welded joints by improvement treatments and prediction of their efficiency. *Zavarivach (Yugoslavia)*. 1987. No. 4. p. 227-231.
27. V.I. Trufyakov, P.P. Mikheev, Yu.F. Kudryavtsev. Surface strengthening of welded joints and prediction of its efficiency. *Rationalisierung im Maschinenbau durch Schlüsseltechnologien. Eigenspannung und Oberflächenverfestigung. DDR. Zwickau*. 1989. p.125-130.
28. V.I.Trufyakov, P.P.Mikheev, Yu.F.Kudryavtsev, D.N.Reznik. Ultrasonic Impact Peening Treatment of Welds and Its Effect on Fatigue Resistance in Air and Seawater. *Proceedings of the Offshore Technology Conference. OTC 7280*. 1993. p.183-193.
29. V.I. Trufyakov, P.P.Mikheev, Yu.F.Kudryavtsev, D.N.Reznik. Review of Fatigue Improvement Treatments and Introduction of Ultrasonic Impact Peening Treatment. *Abstracts of Papers. 74-th AWS Annual Convention*. 1993.
30. V.I.Trufyakov, P.P.Mikheev, Yu.F.Kudryavtsev, D.N.Reznik. Ultrasonic Impact Peening Treatment of Welds. *ABS Fatigue Improvement Seminar. Houston, USA. 30 April, 1993. - 31p*.
31. V.I.Trufyakov, P.P.Mikheev, Yu.F.Kudryavtsev and D.N.Reznik. Fatigue Endurance of Welded Joints. Residual Stresses and Fatigue Improvement Treatments. *Ship Structure Symposium'93. Arlington, Virginia, USA. November 16-17, 1993. p.N1 - N14*.
32. V.I.Trufyakov, P.P.Mikheev, Yu.F.Kudryavtsev. Strengthening Treatment of Welded Joints to Improve Their Fatigue Resistance and Fatigue Life. *TWI Industry Briefing. 13-14 October, 1993. Abington, Cambridge, UK. Paper No. 12, - 10p*.
33. Y. Kudryavtsev, E. Statnikov. Residual Stresses and Fatigue Strength of Welded Joints. *Experimental Studies and Calculation. Proceedings of the International Conference on Fatigue of Welded Components and Structures. Senlis, France. 12 - 14 June, 1996. p. 293 - 300*.

34. V.I.Trufiyakov, P.P.Mikheev, Yu.F.Kudryavtsev, D.N.Reznik. Fatigue endurance of welded joints. Residual stresses and fatigue improvement treatments. IIW Doc. XIII - 1524 - 93. 1993. - 26p.
35. Kudryavtsev Y.F., Trufiyakov V.I., Mikheev P.P., Statnikov E.Sh., Burenko A.G. and Dobykina E.K. Increasing the Fatigue Strength of Welded Joints in Cyclic Compression. International Institute of Welding. IIW DOC.XIII-1569-94. 1994. 5 p.
36. Trufiyakov V.I., Mikheev P.P., Kudryavtsev Y.F. and Statnikov E.Sh. Ultrasonic Impact Treatment of Welded Joints. International Institute of Welding. IIW DOC.XIII-1609-95. 1995.
37. Statnikov E.Sh., Trufiyakov V.I., Mikheev P.P. and Kudryavtsev Y.F. Specification for Weld Toe Improvement by Ultrasonic Impact Treatment. International Institute of Welding. IIW DOC.XIII-1617-96. 1996.
38. Y. Kudryavtsev, J. Kleiman, G. Prokopenko, V. Trufiyakov and P. Mikheev. Ultrasonic Peening of Weldments: Experimental Studies and Computation. IX International Congress on Experimental Mechanics. Orlando. Florida. USA, June 5-8, 2000. p. 504-507.
39. Y. Kudryavtsev, J. Kleiman, G. Prokopenko, P. Mikheev and V. Knysh. Optimum Application of Ultrasonic Peening. SEM Annual Conference and Exposition: Experimental Mechanics in Emerging Technologies. Portland. Oregon. USA, June 4-6, 2001. p. 179-182.
40. Y. Kudryavtsev, J. Kleiman, G. Prokopenko, P. Mikheev and V. Knysh. Mechanism and Efficiency of Ultrasonic Peening in Fatigue Improvement. SEM Annual Conference & Exposition on Experimental and Applied Mechanics. Milwaukee, Wisconsin, USA, June 10-12, 2002 (on CD).
41. S. Roy, J. Fisher and B. Yen. Fatigue Resistance of Welded Details Enhanced by Ultrasonic Impact Treatment (UIT). International Journal of Fatigue.Vol. 25. 2003. p. 1239-1248.
42. X. Cheng, J. Fisher, H. Prask, T. Gnaupel-Heroid, B. Yen and S. Roy. Residual Stress Modification by Post-Weld Treatment and Its beneficial Effect on Fatigue Strength of Welded Structures. International Journal of Fatigue.Vol. 25. 2003. p. 1259-1269.
43. L. Huo, D. Wang, Y. Zhang and J. Chen. Investigation on Improving Fatigue Properties of Welded Joints by Ultrasonic Peening Method. Key Engineering Materials. Trans Tech Publications. Switzerland, 2000, Vols. 183-187, p. 1315-1320.
44. Y. Kudryavtsev, J. Kleiman, V. Knysh and P. Mikheev. Fatigue Life Improvement of Structural Elements with Fatigue Cracks. SEM Annual Conference & Exposition on Experimental and Applied Mechanics. Milwaukee, Wisconsin, USA, June 10-12, 2002. (on CD)
45. Y. Kudryavtsev, J. Kleiman, G. Prokopenko, B. Mordiyuk, T. Krasovskiy P. Mikheev and V. Knysh. Computerized Complex for Ultrasonic Peening of Parts and Welded Elements. 32-nd Annual Ultrasonic Industry Association Symposium. New York, NY, USA, October 21-23, 2002. (on CD)
46. Patent of USA # 6467321. 2002. Device for Ultrasonic Peening of Metals. George I. Prokopenko, Jacob I. Kleiman, Oleksandr I. Kozlov, Pavel P. Micheev, Vitaly V. Knysh, Yuriy F. Kudryavtsev.
47. Y. Kudryavtsev, J. Kleiman and O. Gushcha. Residual Stress Measurement in Welded Elements by Ultrasonic Method. IX International Congress on Experimental Mechanics. Orlando. Florida. USA, June 5-8, 2000. p. 954-957.